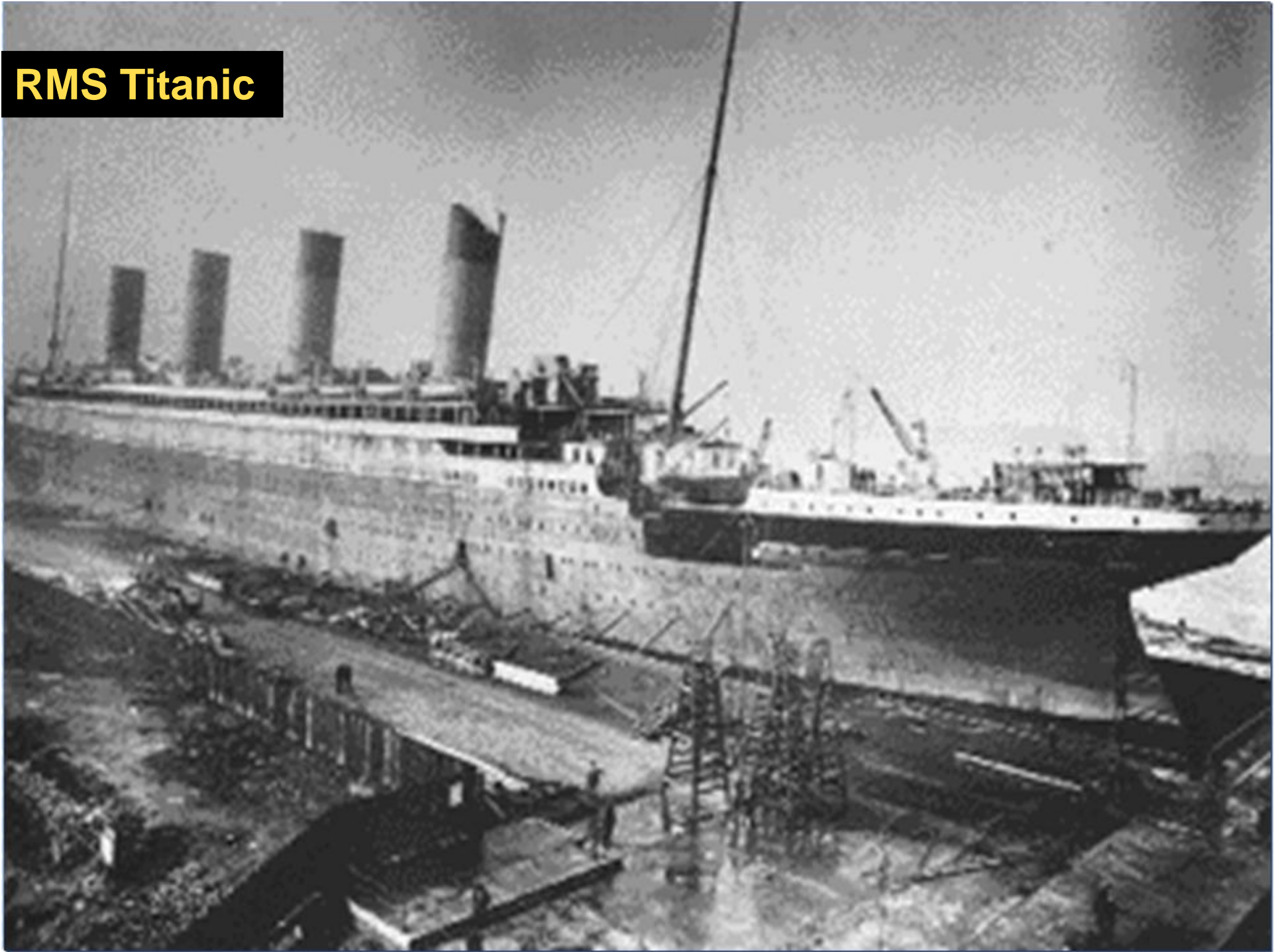


Ductile-to-brittle transition temperature (DBTT) in steels and its significance in design and manufacturing

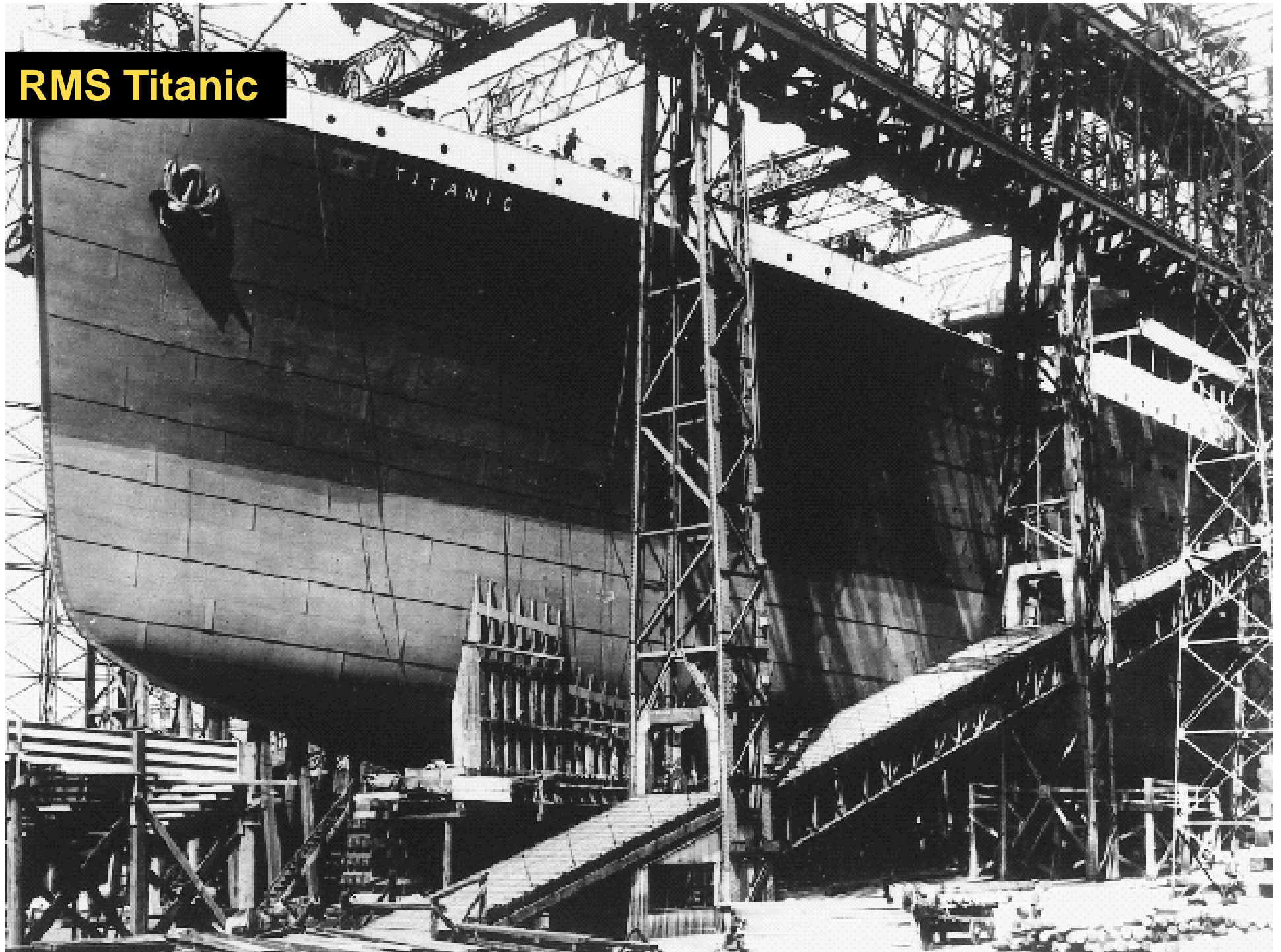
By: Kamran Khodaparasti

Tehran, June 2009

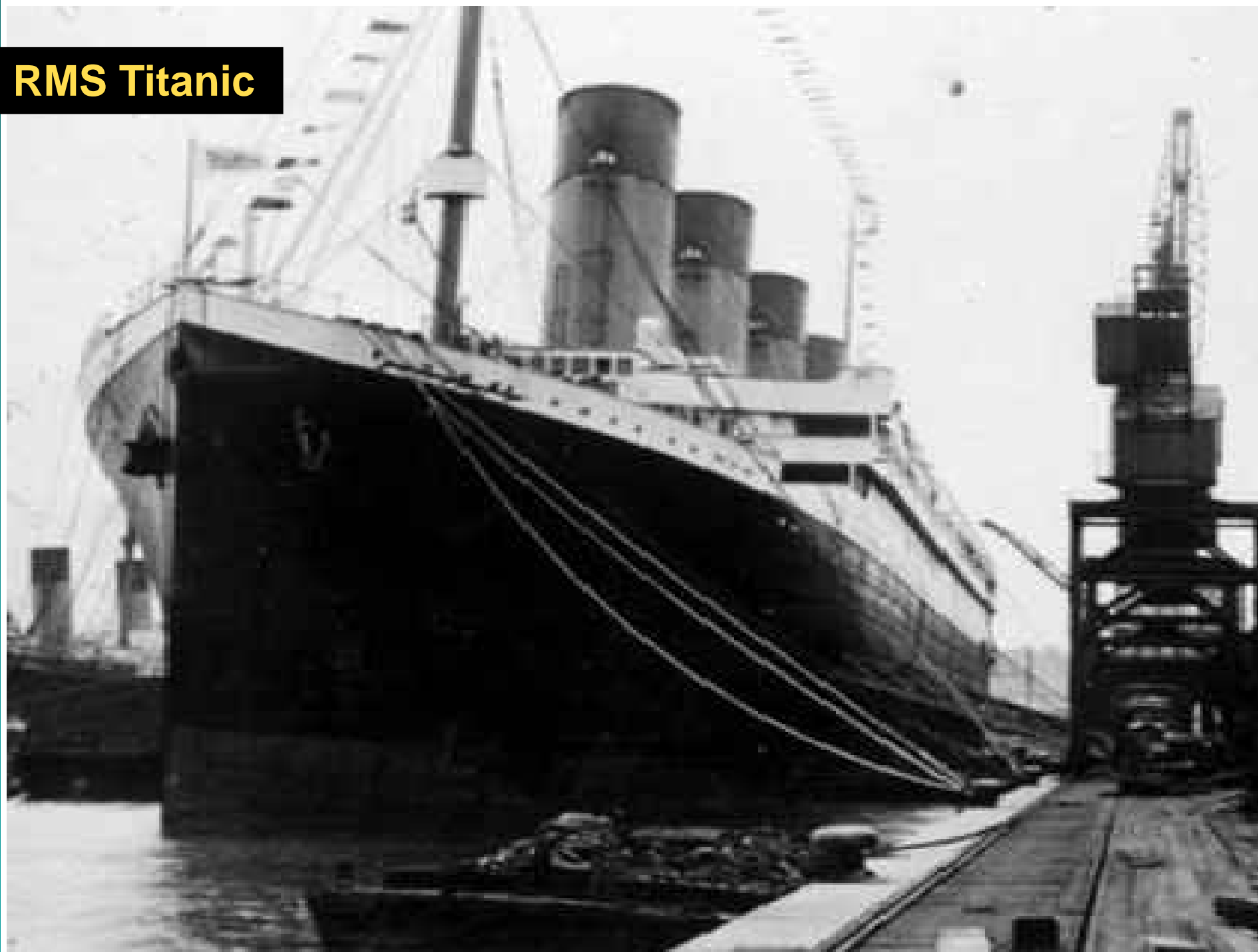
RMS Titanic



RMS Titanic



RMS Titanic



RMS Titanic



Titanic features



RMS Titanic, April 14, 1912

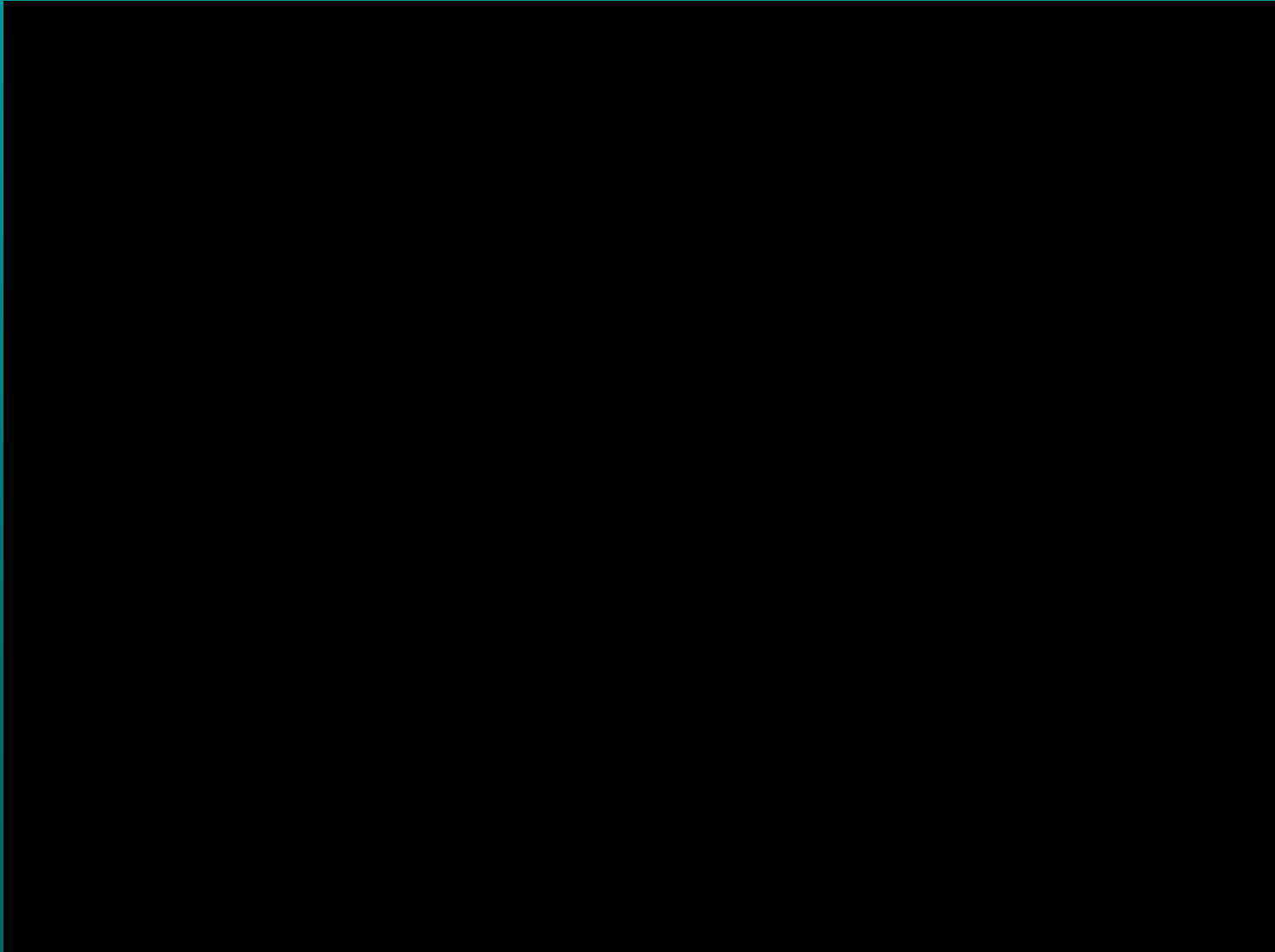




Titanic sinking



Rediscovery of the Titanic (Possible factors in the sinking)



World War II emergency ship building program (USA)

Ships production over the years 1941-1946 :

- n 2580 Liberty ships
- n 414 Victory ships
- n 530 T2 oil tankers

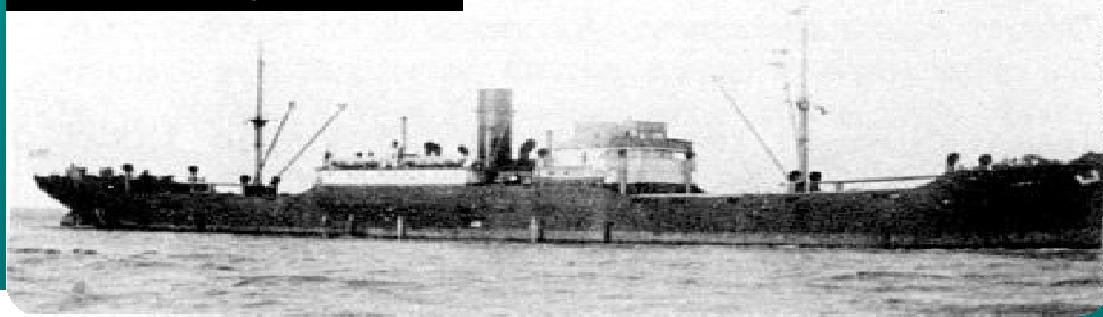
Towards the end of the program one ship was completed in less than five days.



Between 1942 and 1952:

- n 250 large welded steel ships were lost
- n Another 1200 welded ships suffered relatively minor damage (cracks less than 3 m long)

SS Liberty



T2 oil tanker



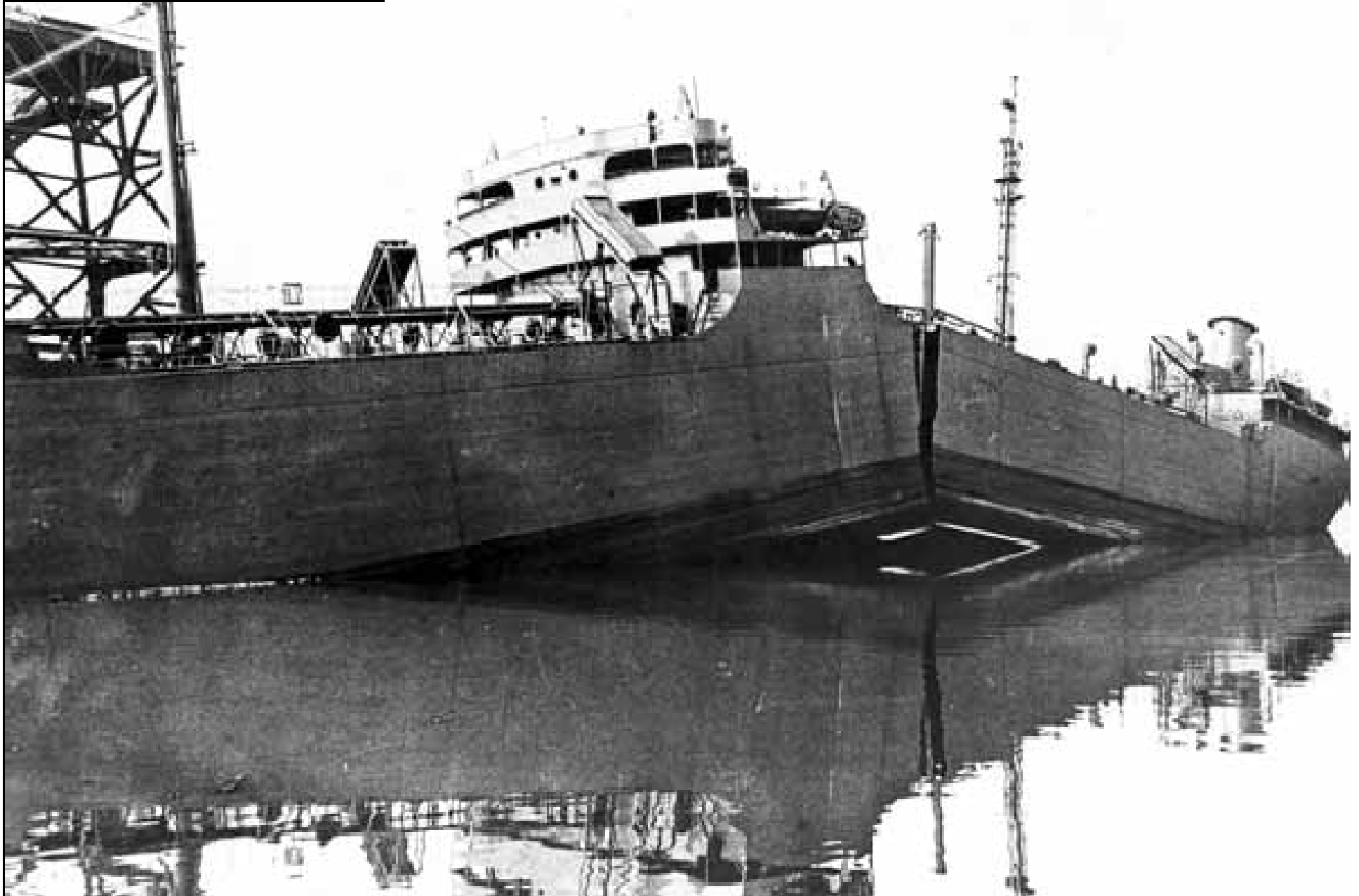
Fracture at sea



Fracture at dock



Fracture at dock



Over 58 cases of non-ship failures had been reported

- n Storage tanks and pressure vessels
- n Offshore structures
- n Bridges
- n Pipe lines
- n ...

Floating roof tank, Esso
Fawley Refinery, 1952



What is the problem?

Year	Structure	Temp at failure / °C	Steel thickness / mm	Age of structure / years
1904	Water tank	0	15.9	7
1925	Oil storage tank	-20	25.4	-
1940	Trussed bridge	-14	52	2-3
1943	Liberty ships	2	-	≤1
1951	Plate girder bridge	-1	63	3
1952	Oil/gas storage tank	8	27	-
1954	Post office building	1	15-25	0



Rivet or weld?

Please wait...

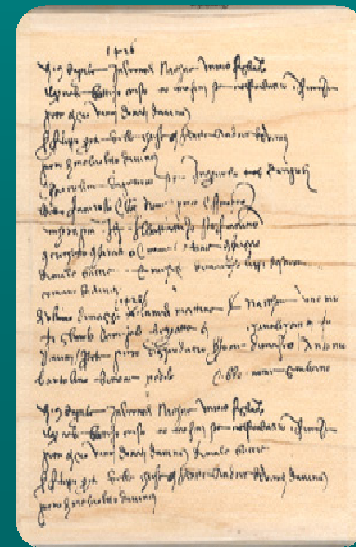
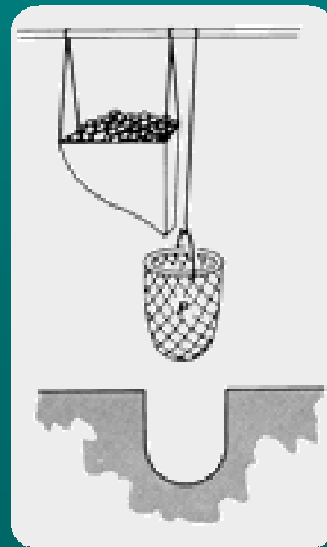
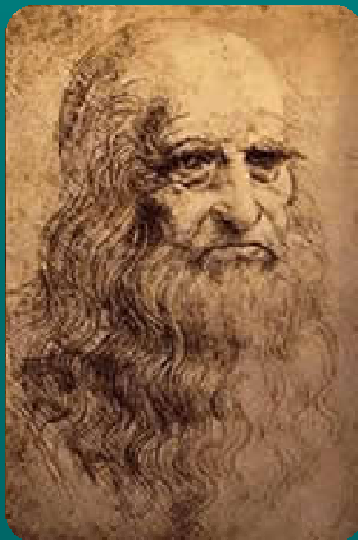


Properties of materials

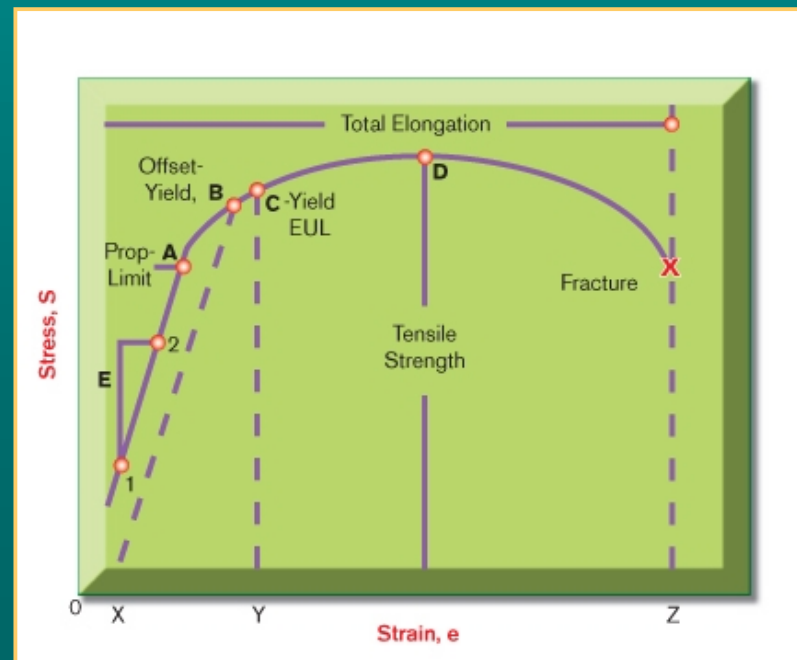
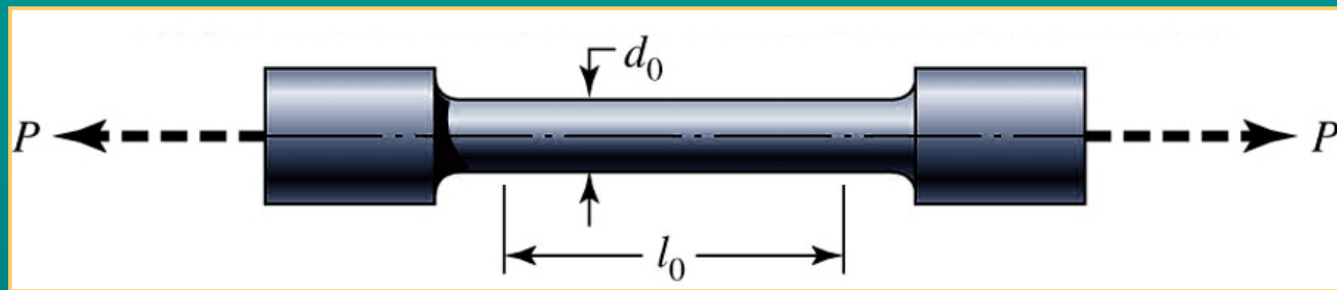
- n Mechanical properties → tension test
- n Electrical properties → compression test
- n Magnetic properties → impact test
- n Optical properties → hardness test
- n Corrosion properties → creep test
- n Biological properties → ...
- n ...

Tension test

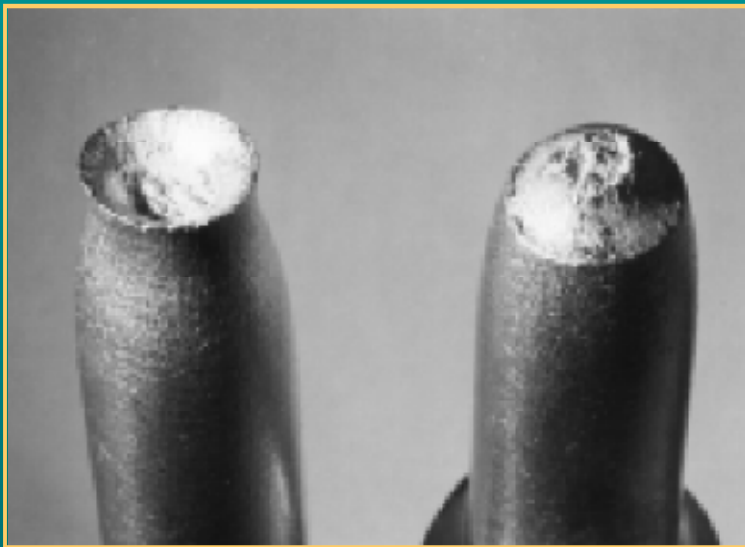
- n Leonardo Da Vinci, 1495 (500 yrs ago!) observed:
the longer the wire, the smaller the load for failure
- n Reasons:
 - flaws cause premature failure
 - Larger samples contain more flaws!



Tension test (static material test)



Fracture type

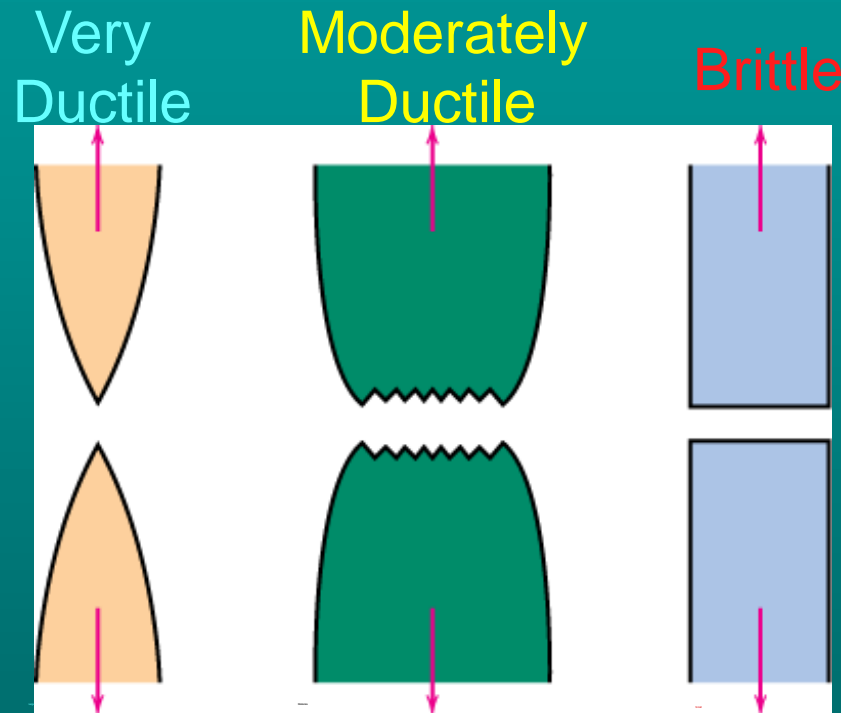


Ductile fracture
(cup-and-cone)



Brittle fracture

Ductile fracture is desirable!

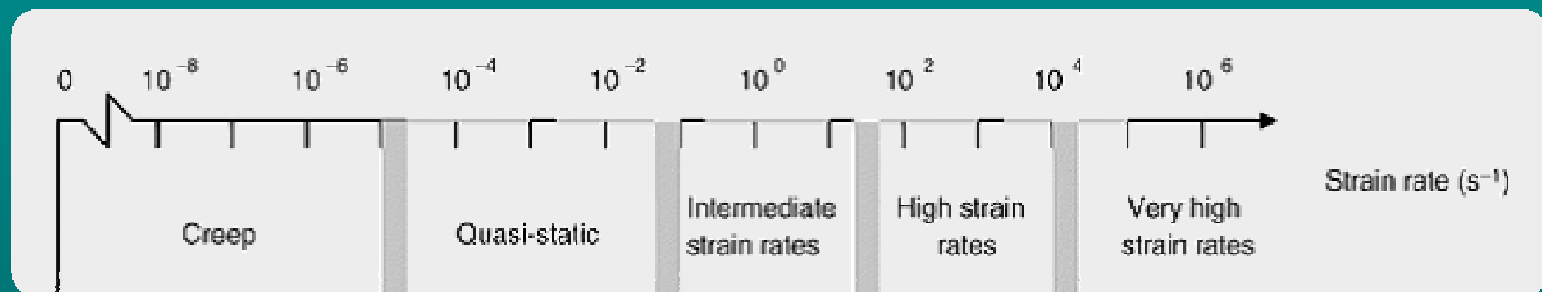


Ductile:
warning before fracture

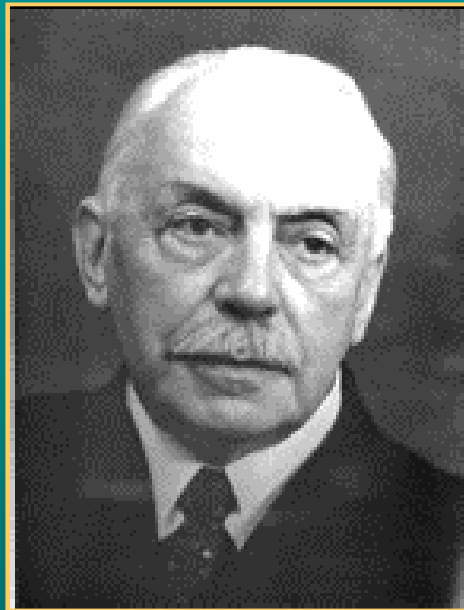
Brittle:
No warning

Loading

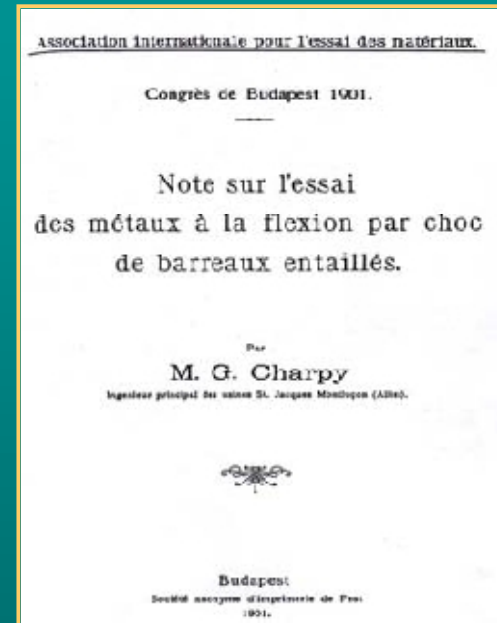
- n Static loading (Low strain rate) $10^{-1} - 10^{-5} \text{ (S}^{-1}\text{)}$
- n Dynamic loading (High strain rate) $10^{+x} \text{ (S}^{-1}\text{)}$



Impact test (dynamic material test)



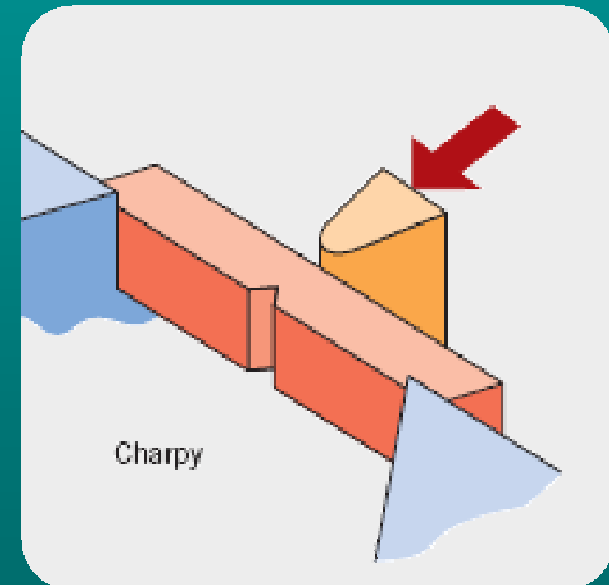
Augustin Georges Albert Charpy
(1865 – 1945), Paris



Title page of Charpy's paper
at the VIIth Congress of the International
Assoc. For Testing of Materials in
Budapest, 1901

Charpy impact test

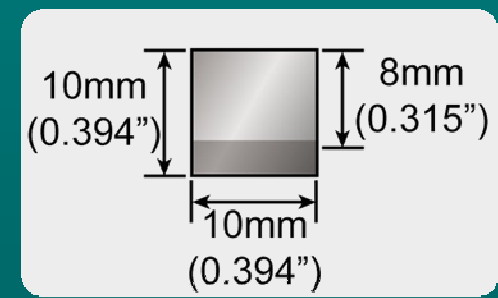
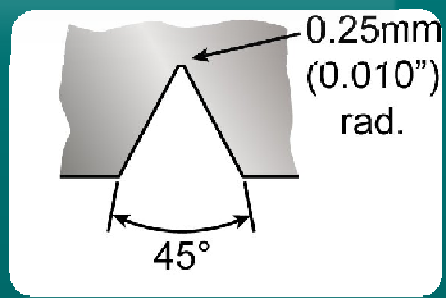
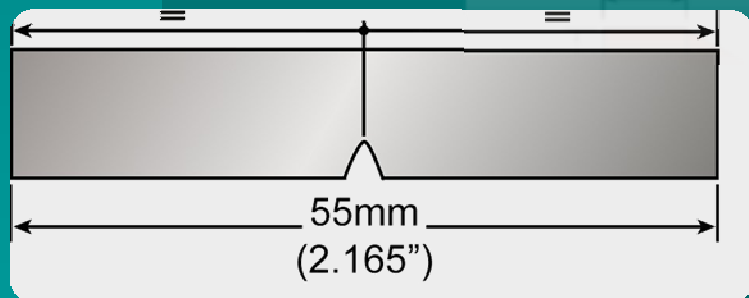
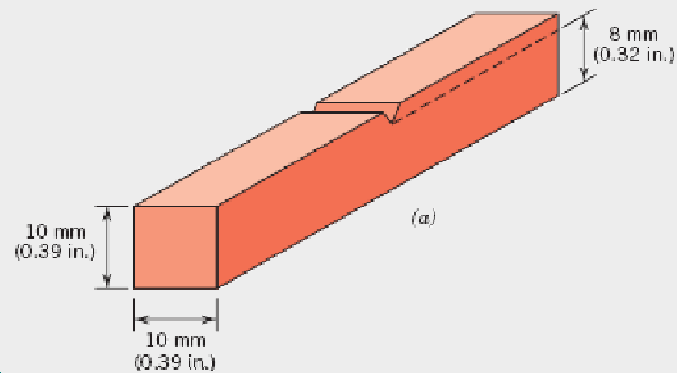
- n ASTM E 23
- n Impact test velocity is ~ 5 m/s



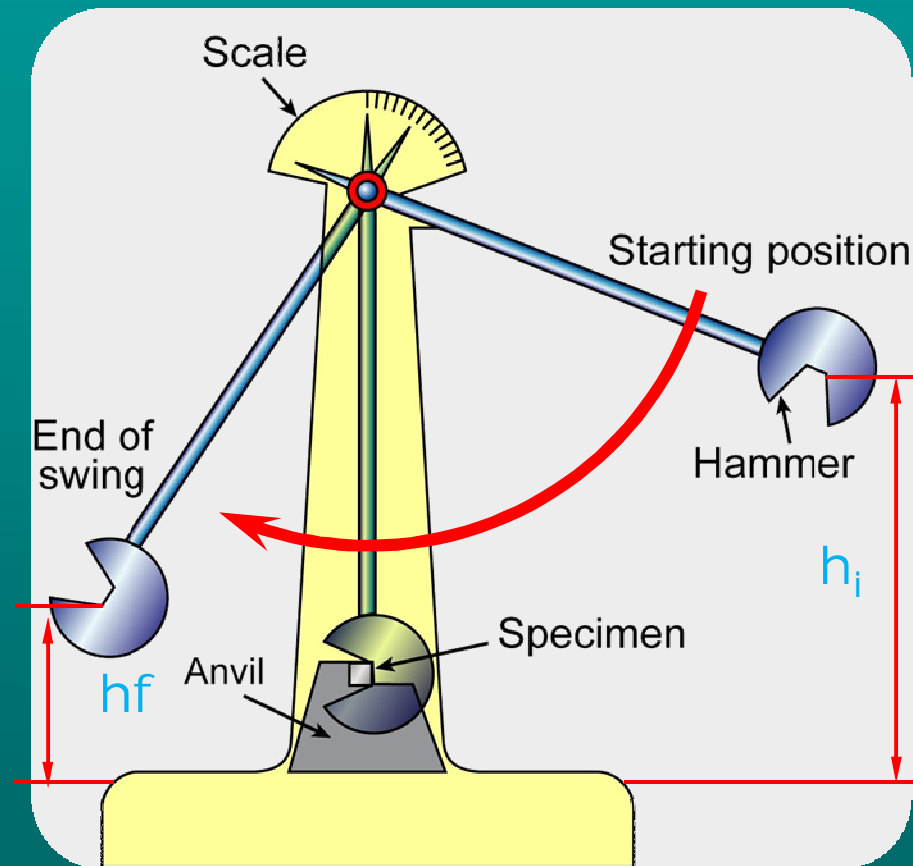
Impact test machine



Charpy V-notch impact test specimen



Charpy V-notch impact test



$$\text{Fracture energy} = mgh_i - mgh_f$$

Charpy impact test

100% Brittle

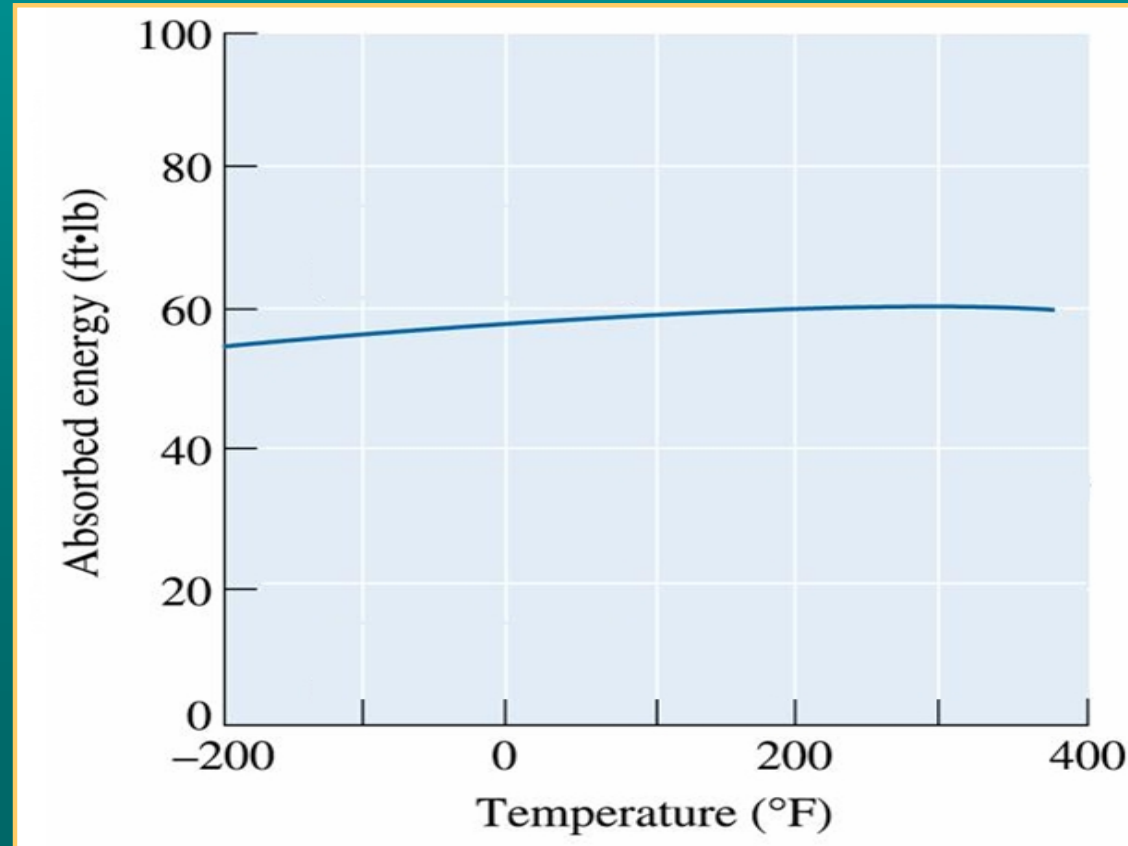


100% Ductile



Impact test graph

- n More absorbed energy → More ductility



Let's get back to our story!



How can I find
the answer ?



A broad research program

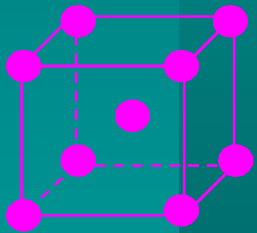
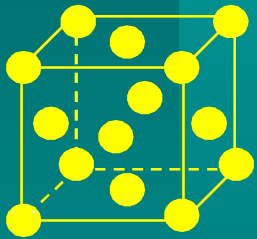
- n To find the causes of this failures
- n Gaining a better understanding of the mechanism of brittle fracture and fracture in general



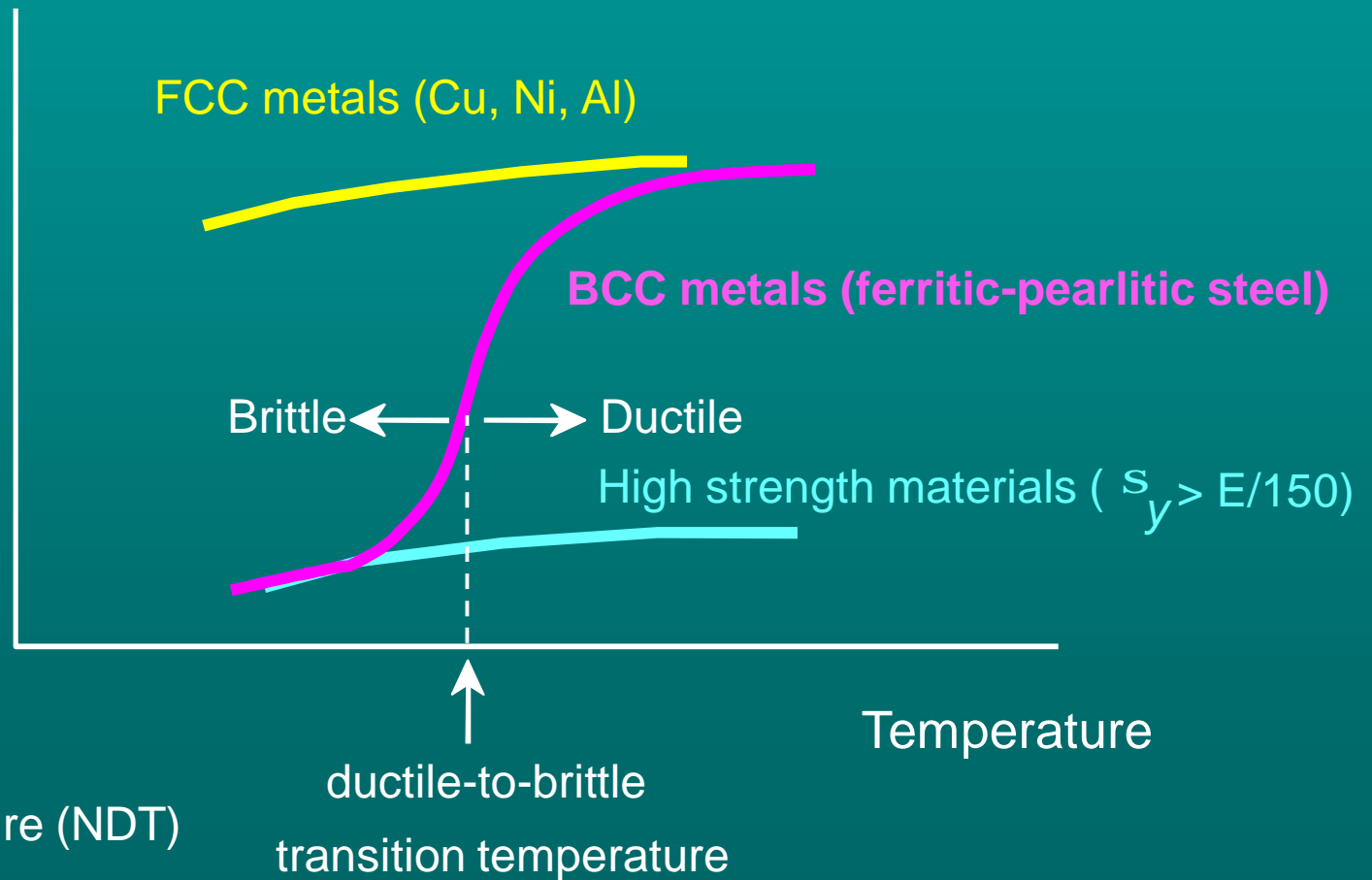
The U.S. National Bureau of Standards' report (Williams et al. 1948)

- n The NBS study included:
 - Chemical analysis
 - Tensile tests
 - Microscopic examination
 - Charpy impact tests
- n The Notable conclusions of the report:
 - The plates in which the fracture arrested had consistently higher impact energies and lower transition temperatures than those in which the fractures originated.
 - There was no similar correlation with chemical composition, tensile properties or microstructure

Ductile-to-Brittle Transition Temperature (DBTT)...

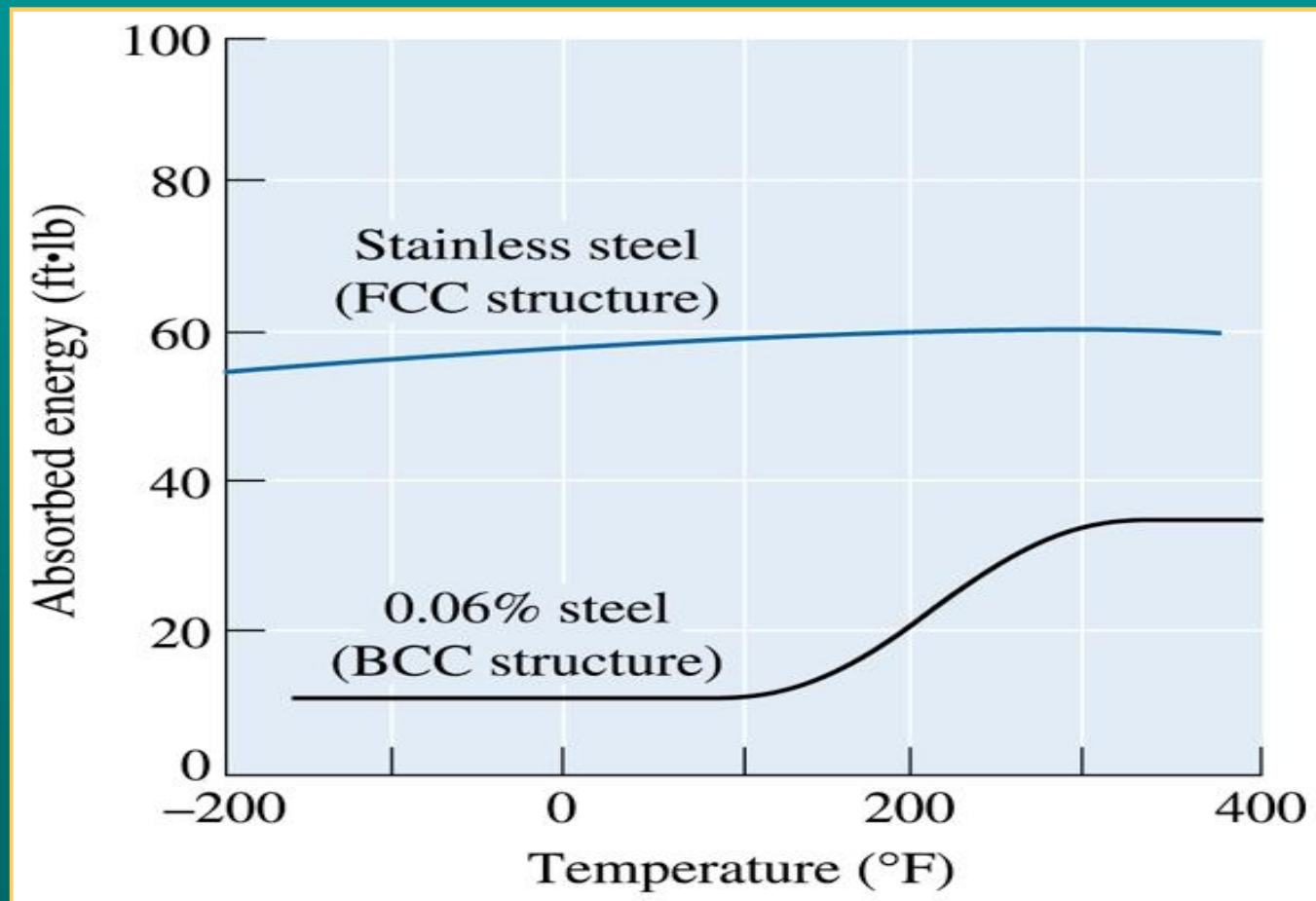


Impact Energy

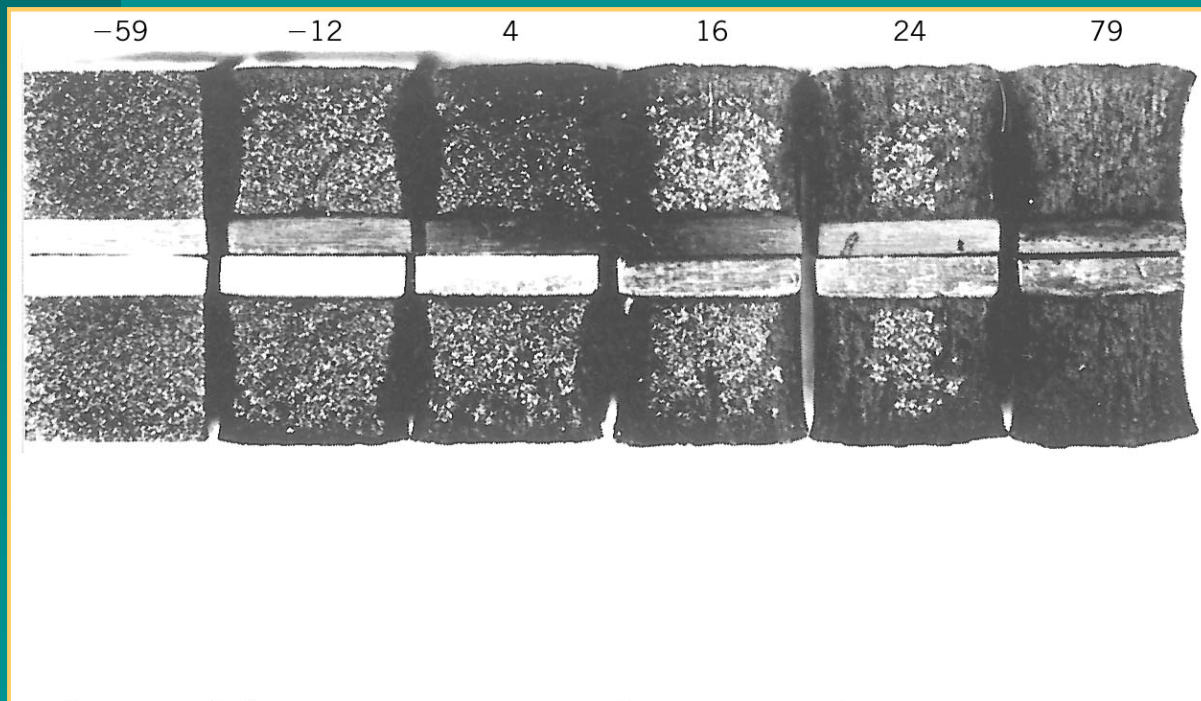


Nil ductility temperature (NDT)

Some examples...



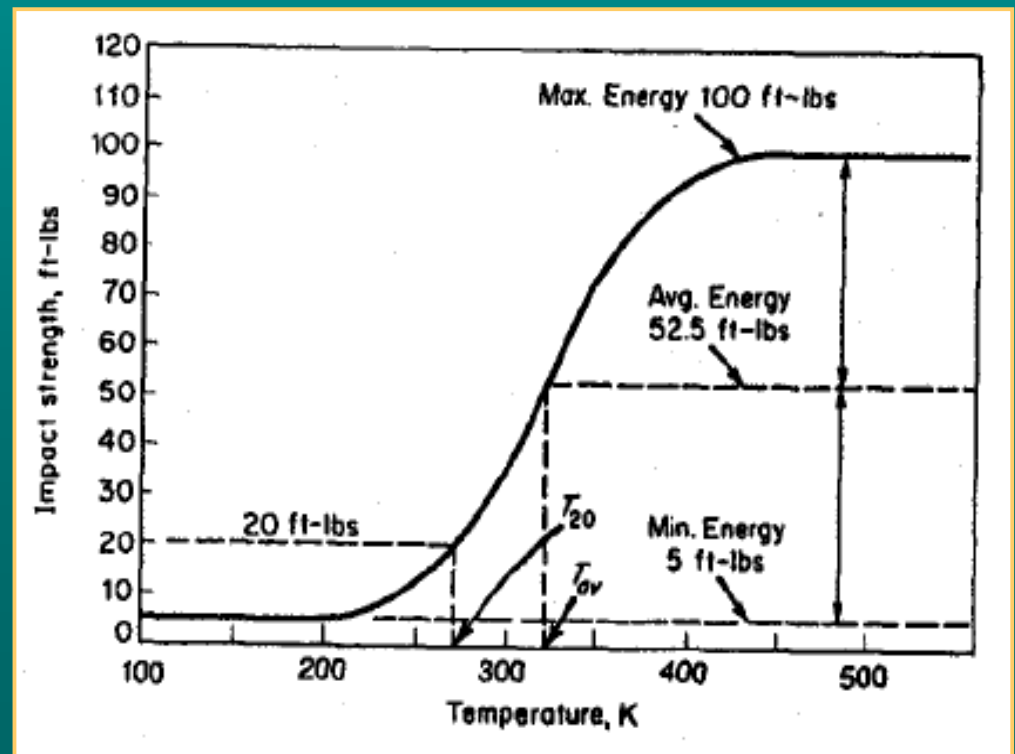
Fracture surface



fracture surfaces of A36 steel Charpy V-notch specimens tested at indicated temperatures (in °C).

Criterion for transition temperature

- n Ductility transition temperature (T_{20} in the figure)
- n Average temperature (T_{av} in the figure)



1ft-lb = 1.4 J

Why?

- n In FCC metals, the flow stress, i.e. the force required to move dislocations, is not strongly temperature dependent. Therefore, dislocation movement remains high even at low temperatures and the material remains relatively ductile
- n The yield stress or critical resolved shear stress of BCC crystals is markedly temperature dependent, in particular at low temperatures
- n The temperature sensitivity of the yield stress of BCC crystals has been attributed to the presence of interstitial impurities on the one hand, and to a temperature dependent Peierls-Nabarro force on the other



Ductile-to-brittle transition



How can I
control this
phenomenon ?

Metallurgical factors affecting transition temperature

Changes in transition temperature of over 50 °C can be produced by changes in :

- n Chemical composition
- n Microstructure
- n Heat treatment

Effect of chemical composition

- n The largest changes result from changes in the amount of carbon and manganese.

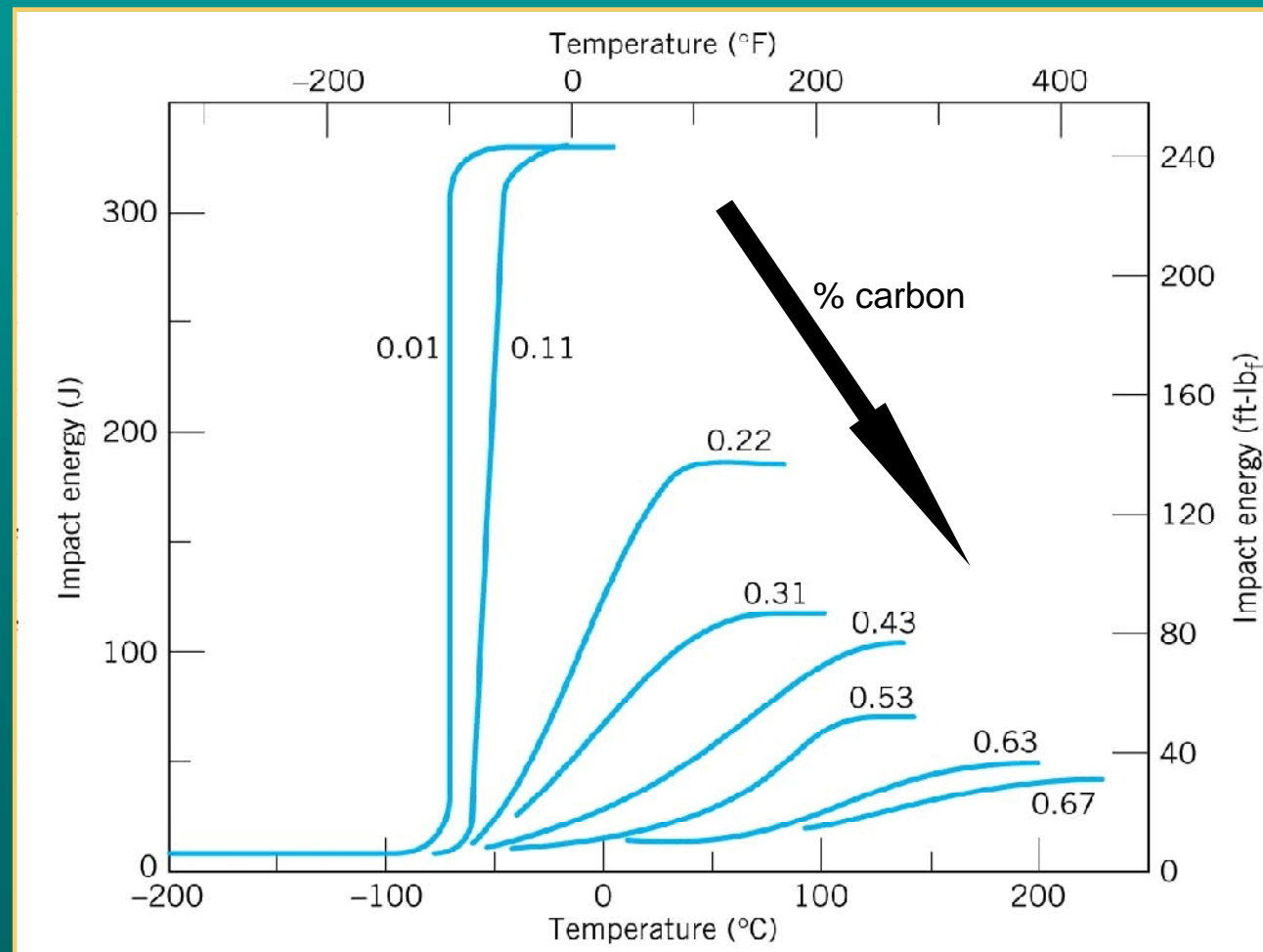
0.1% C 

0.1% Mn 


14 °C  DBTT

5 °C  DBTT

Effect of carbon



Note that...

- n The **Mn:C** ratio should be at least 3:1 for satisfactory notch toughness
- n A higher **Mn:S** ratio reduces the ductile-brittle transition temperature substantially
-  n When the **oxygen** content was raised from 0.001% to the high value of 0.057%, the transition temperature was raised from -15 °C to 340 °C !!
- n In view of this results, it is not surprising that **deoxidation** practice has an important effect.

Type of steels

- n **Rimmed** steel , with its high iron oxide content, generally shows a transition temperature above room temperature
- n **Semikilled** steels, which are deoxidized with Si, have a lower transition temperature
- n For steels which are **fully killed** with Si + Al the ductility transition temperature will be $-60\text{ }^{\circ}\text{C}$

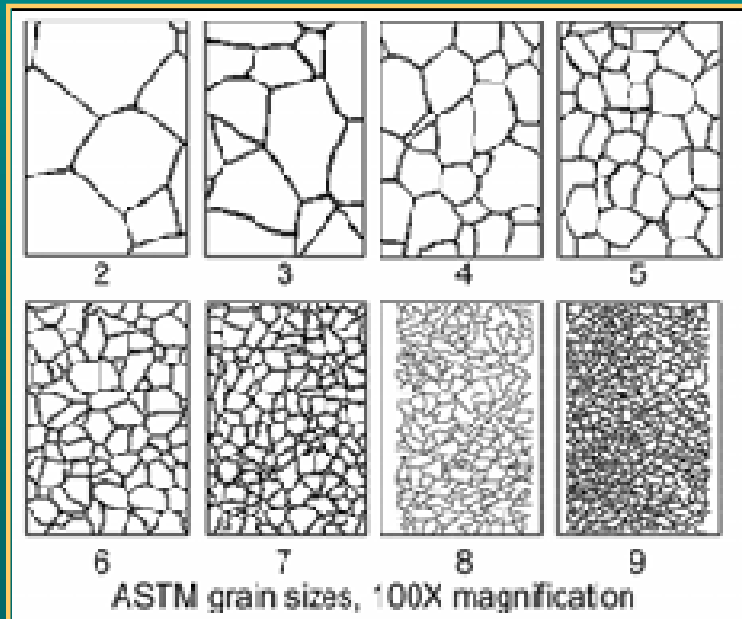
Effect of other elements



- n The role of **nitrogen** is difficult to assess because of its interaction with other elements but generally considered to be detrimental.
- n **Silicon** > 0.25% raise the transition temperature.
- n **Molybdenum** raises the transition temperature almost as rapidly as carbon.
- n The transition temperature decreases about 40 °C per 0.1% **aluminum** added. However, additions of aluminum greater than that required to tie up the nitrogen have little effect.

Effect of microstructure

- n Grain size has a strong effect. An increase of one ASTM number (actually a decrease in grain diameter) can result in a decrease in transition temperature of 15 °C for mild steel.



ASTM Grain Size Number	Number of Grains per Square Inch at 100X	Average Grain Diameter (10^{-6}m)
1	1	254
2	2	180
3	4	127
4	8	90
5	16	64
6	32	45
7	64	32
8	128	22.4
9	256	15.9
10	512	11.2

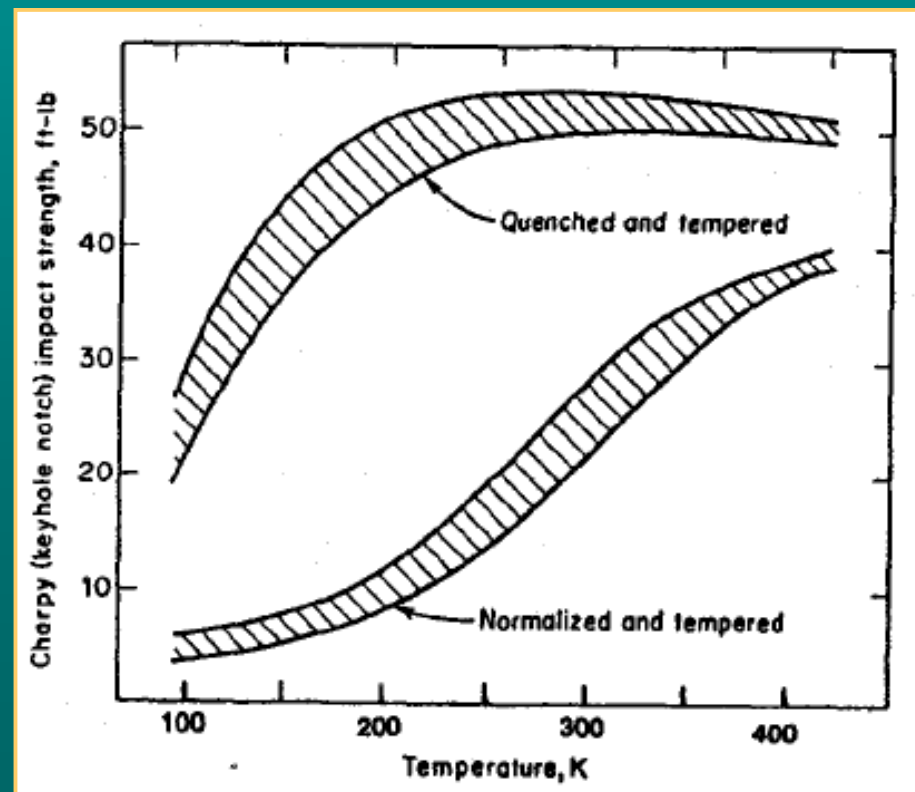
ASTM E 112

Blue line ~ grain of salt size
Red line ~ diameter of human hair

Effect of Heat Treatment

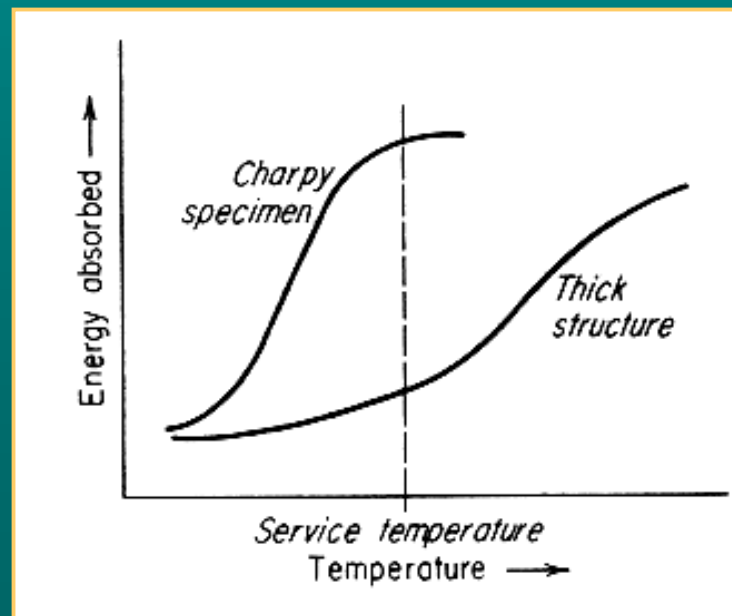
- n Heat treatment, through its influence on microstructure, has a strong effect on impact properties.

Both heat treatments produce the same hardness but widely different DBTT



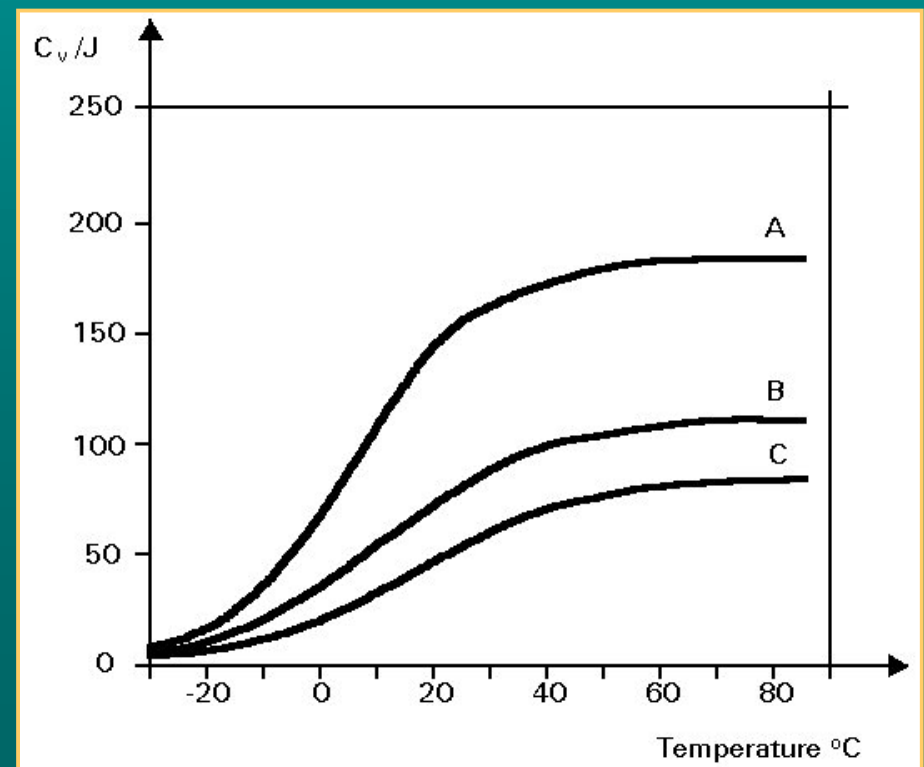
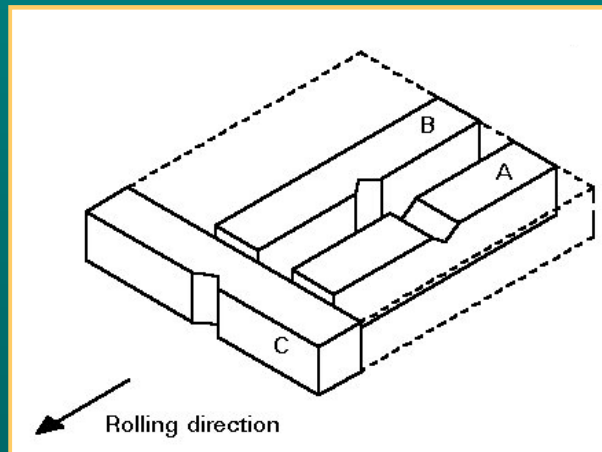
Other factors affecting transition temperature

- n For a given chemical composition and deoxidation practice, the transition temperature will be appreciably higher in thick hot-rolled plates than in thin plates ($t > 13$ mm). This is due to the difficulty of obtaining uniformly fine pearlite and grain size in a thick section.

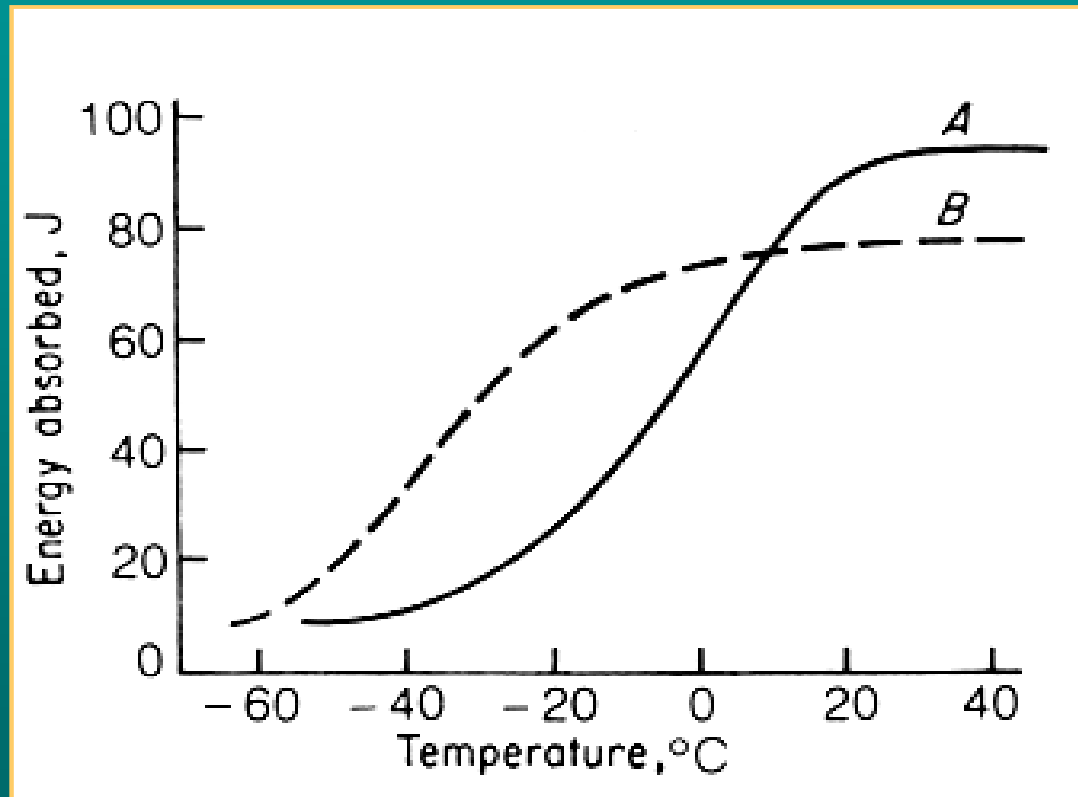


Other factors affecting transition temperature

- n The notched-impact properties of rolled or forged products vary with orientation in the plate or bar.



Error in judgment?



Transition temperature curve for two steels showing fallacy of depending on room temperature results.

RMS Titanic: Did a metallurgical failure cause a night to remember?



The bow of the Titanic as it appeared during 1986 expedition

Chemical analysis

- n Comparing the composition of the Titanic steel and ASTM A36 steel shows that the modern steel has a higher manganese content and lower sulfur content, yielding a higher Mn:S ratio that reduced the ductile-brittle transition temperature substantially. In addition, ASTM A36 steel has a substantially lower phosphorus content, which will also lower the ductile-to-brittle transition temperature.

Table II. The Composition of Steels from the *Titanic*, a Lock Gate, and ASTM A36 Steel

	C	Mn	P	S	Si	Cu	O	N	MnS: Ratio
<i>Titanic</i> Hull Plate	0.21	0.47	0.045	0.069	0.017	0.024	0.013	0.0035	6.8:1
Lock Gate*	0.25	0.52	0.01	0.03	0.02	—	0.018	0.0035	17.3:1
ASTM A36	0.20	0.55	0.012	0.037	0.007	0.01	0.079	0.0032	14.9:1

*Steel from a lock gate at the Chittenden ship lock between Lake Washington and Puget Sound, Seattle, Washington.

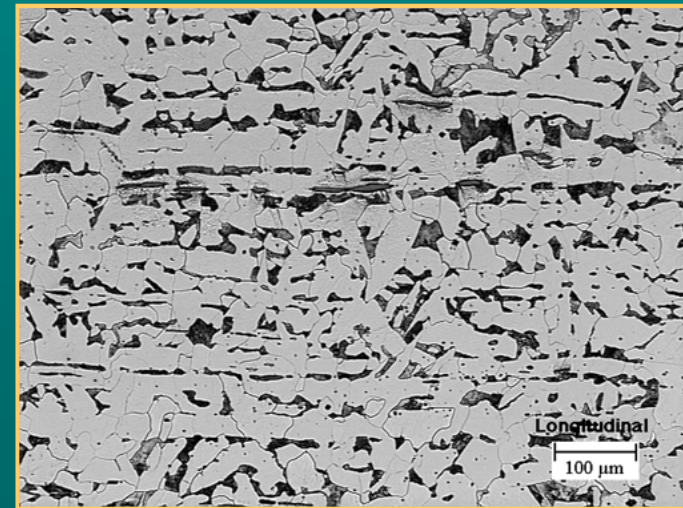
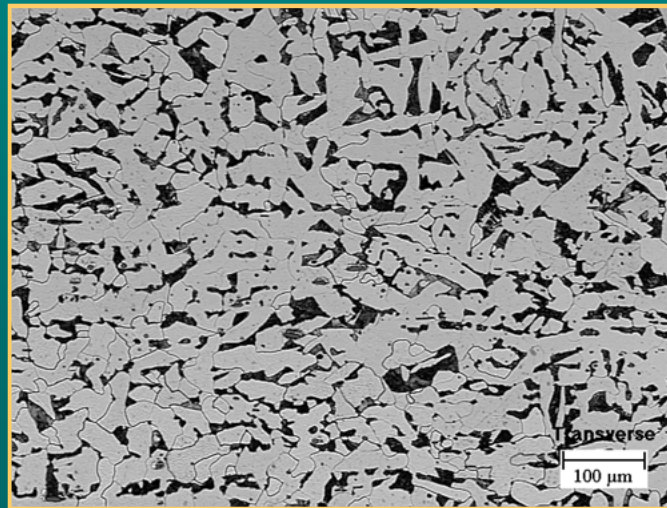
Tension test

Table III. A Comparison of Tensile Testing of *Titanic* Steel and SAE 1020

	<i>Titanic</i>	SAE 1020
Yield Strength	193.1 MPa	206.9 MPa
Tensile Strength	417.1 MPa	379.2 MPa
Elongation	29%	26%
Reduction in Area	57.1%	50%

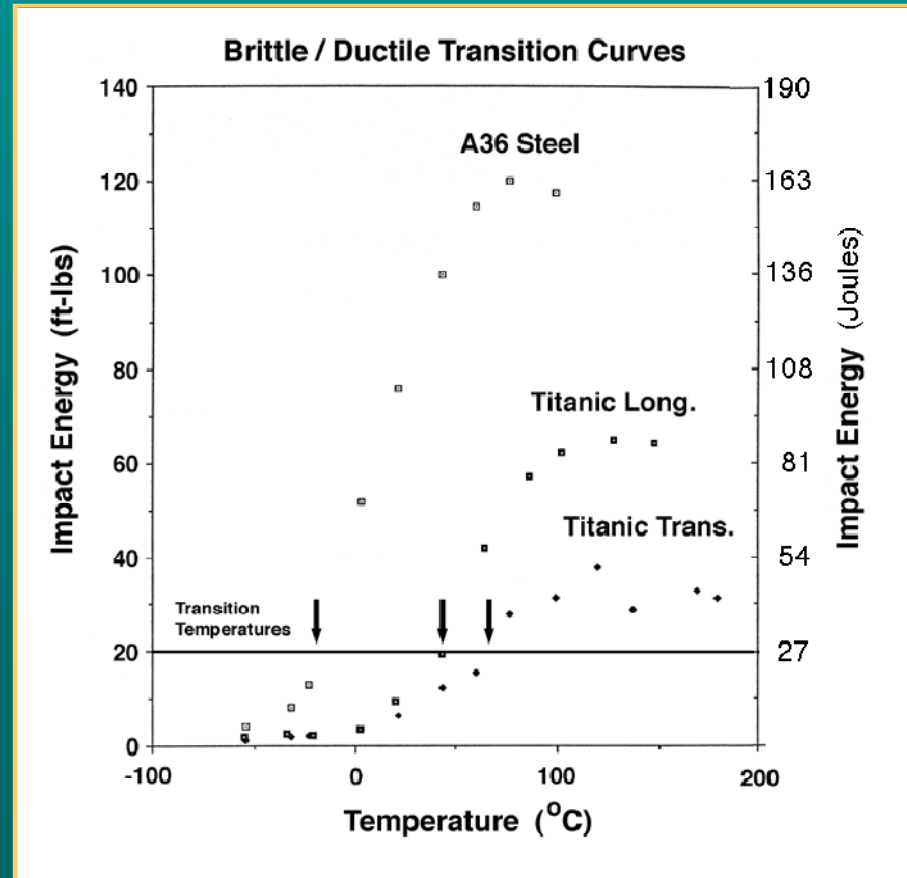
Metallography

- n An optical micrograph of steel for the hull of the Titanic in (right) longitudinal and (left) transverse directions, showing banding that resulted in elongated pearlite colonies and MnS particles. Etchant is 2% Nital.



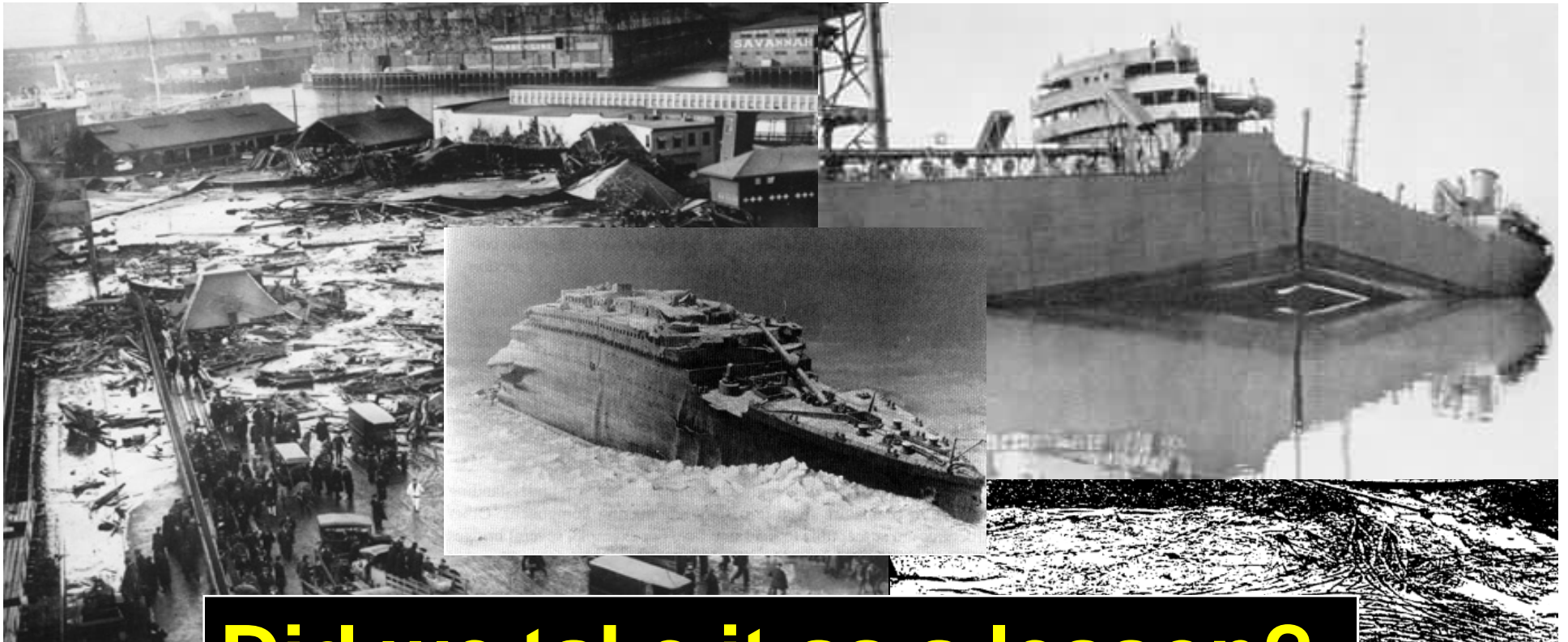
DBTT

- n The ductile-brittle transition temperature for the longitudinal specimens was 33°C .

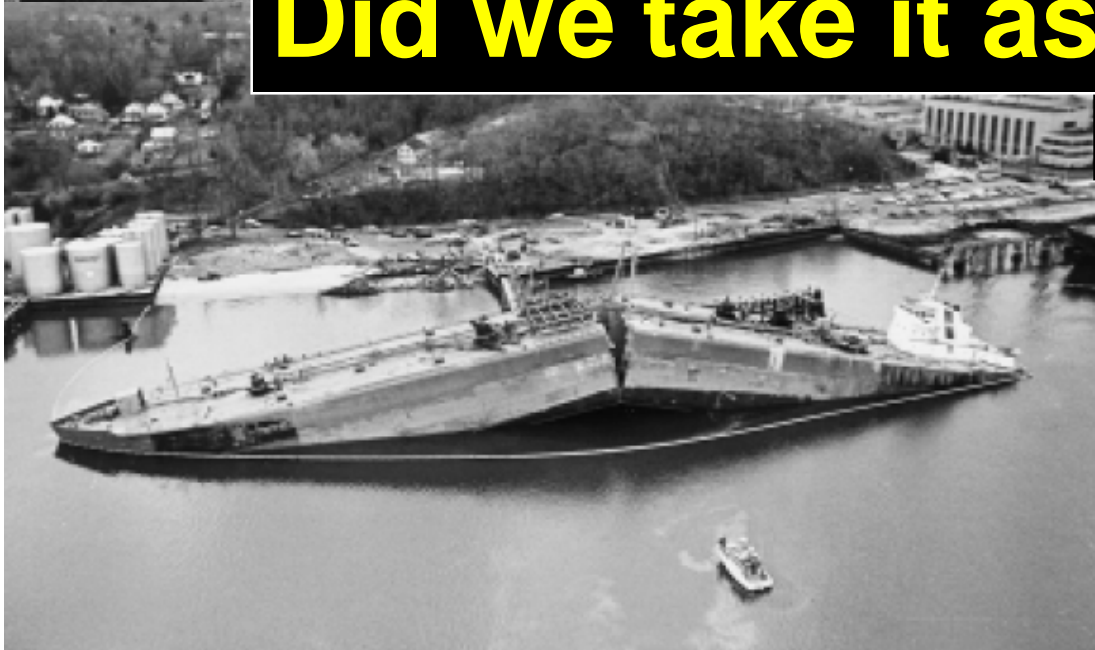


Conclusions

- n The steel used to construct the Titanic's hull, though adequate in strength, possessed a high DBTT (at the time of the collision, the sea water temp. was $-2\text{ }^{\circ}\text{C}$)
- n The low toughness was likely due to a complex combination of factors, including low Mn content, a low Mn:C ratio, a large ferrite grain size and large and coarse pearlite colonies.
- n The steel used was probably the best plain carbon ship plate available at the time of the ship's construction.

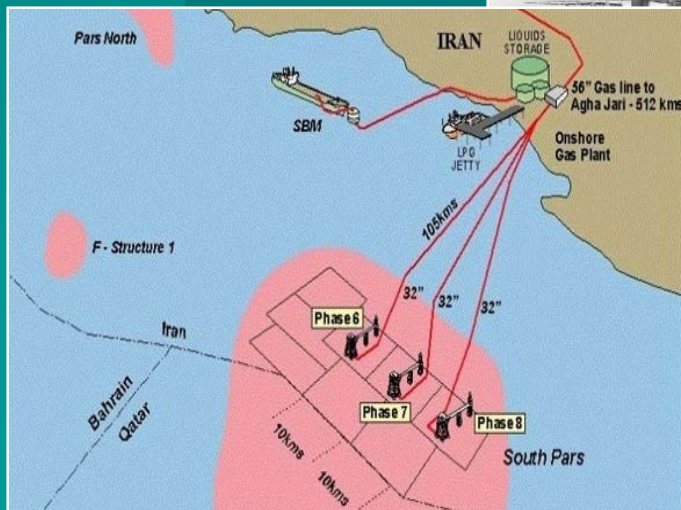


Did we take it as a lesson?



n Did we take it as a lesson?

South of Iran



Offshore drilling rig, "Sea Gem", December 27, 1964



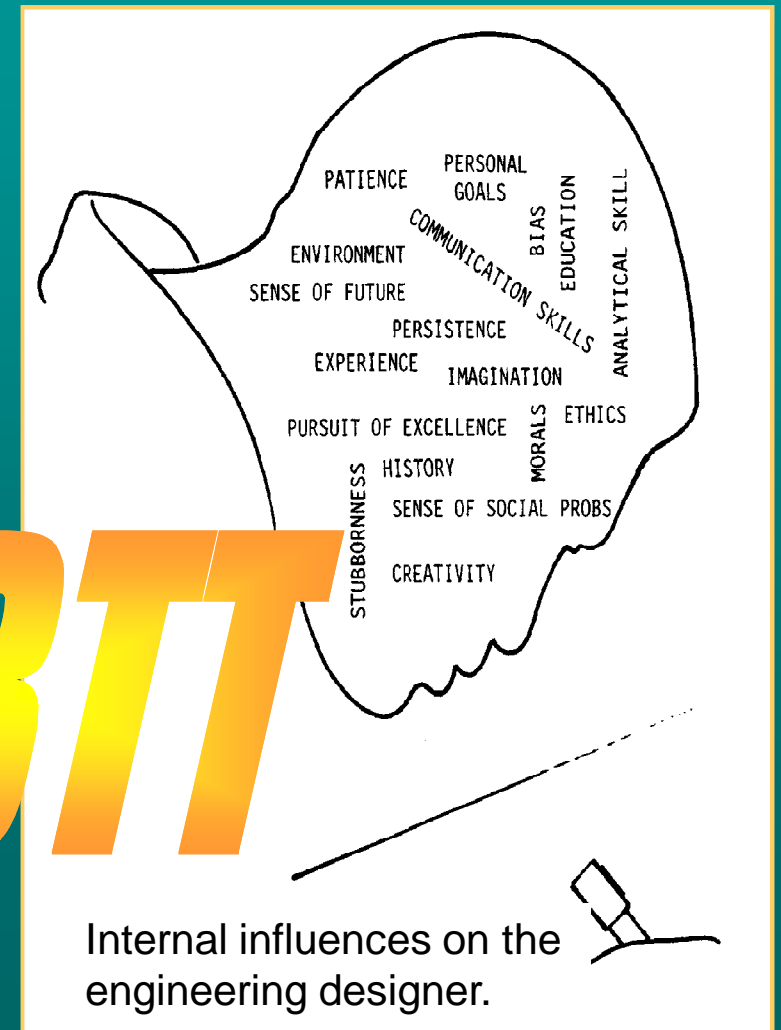
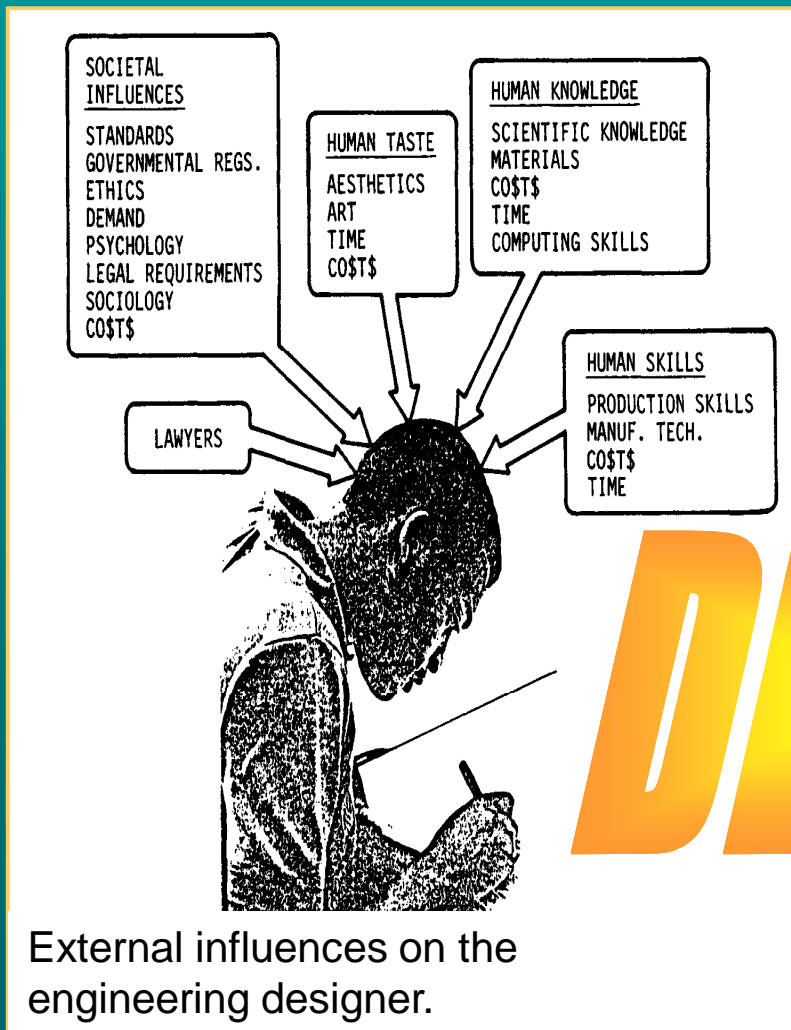
Robert Jenkins pressure vessel, November 6, 1970



DANGER IS EVERYWHERE

DESIGN STRATEGY: STAY ABOVE THE DBTT!

I hope...





Thanks for your attention